

# **Ignition of Solid Fuels and the Modelling of Forest Fires**

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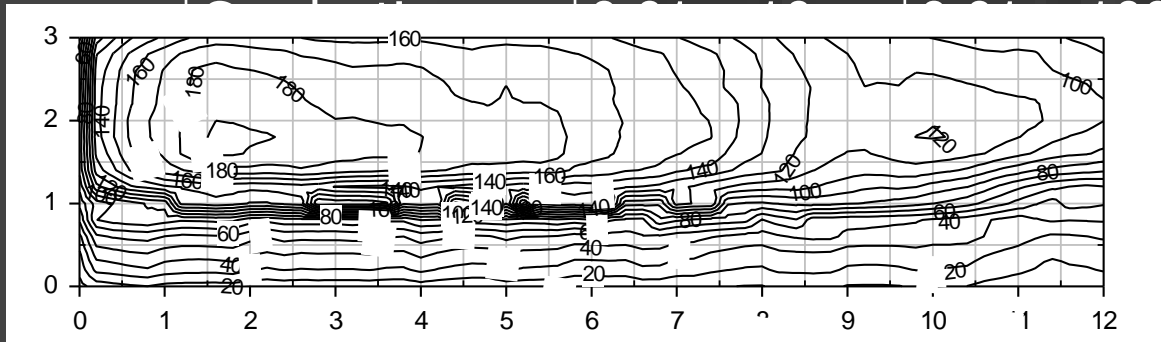
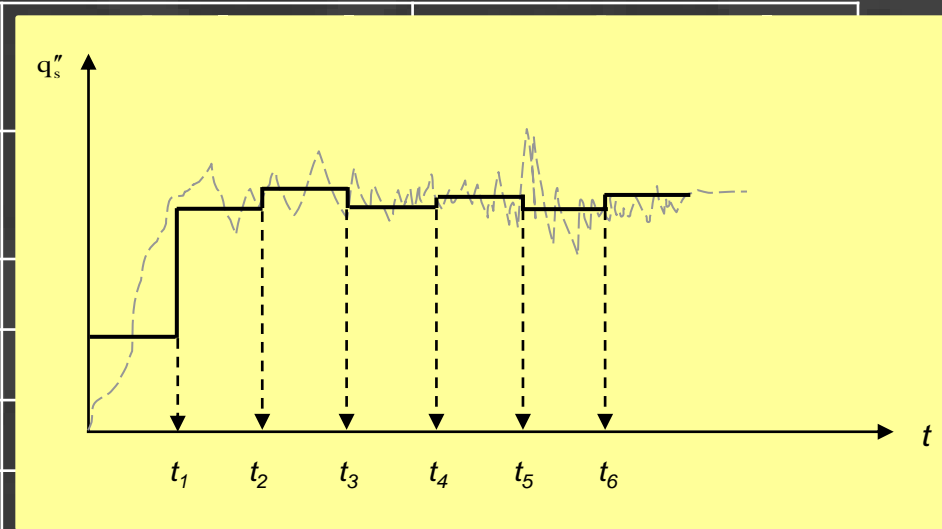
**BRE Centre for Fire Safety Engineering**

**The University of Edinburgh, UK**

# Modelling of Forest Fires

o A very complex problem

Type	Time Scale (s)
Combustion	0.0001 – 0.01
Fuel particles	-
Fuel complex	-
Flames	0.1 – 30
Radiation	0.1 – 30



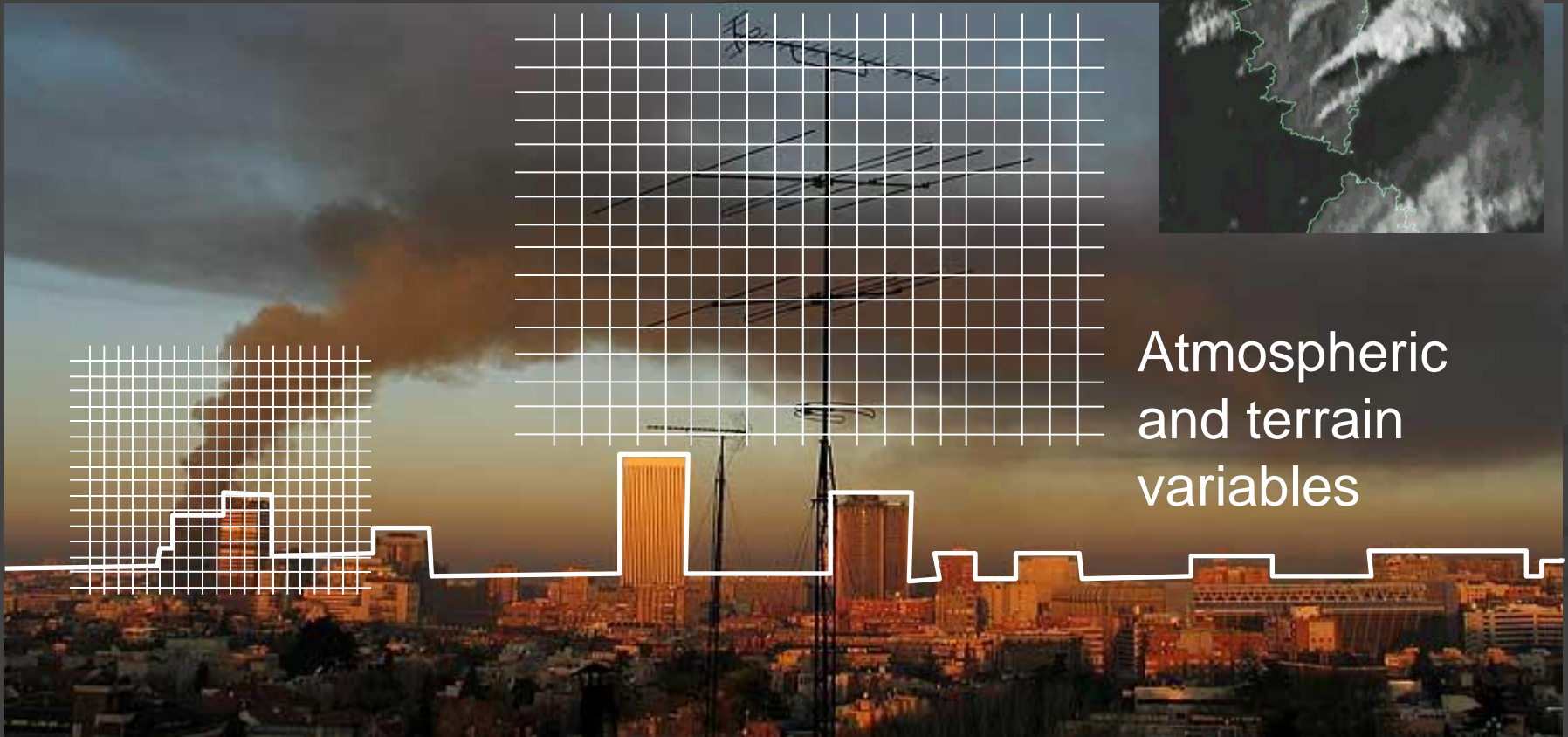
0.01 – 0.1
0.1 – 10
1 – 1,000
1 – 10,000
1 – 100

Sullivan, A., "A Review of Wildland Fire Spread Modelling, 1990-Present, 1: Physical and Quasi-Physical Models", arXiv:0706.3074v1[physics.geo-ph] (2007).

# Compatibility

- Resolving all length and time scales in a single model is impossible
- It is necessary to develop sub-grid/filtering models
- Sub-grid/filtering models need to be “**compatible**” with the outputs of the primary model

# Atmospheric Scale



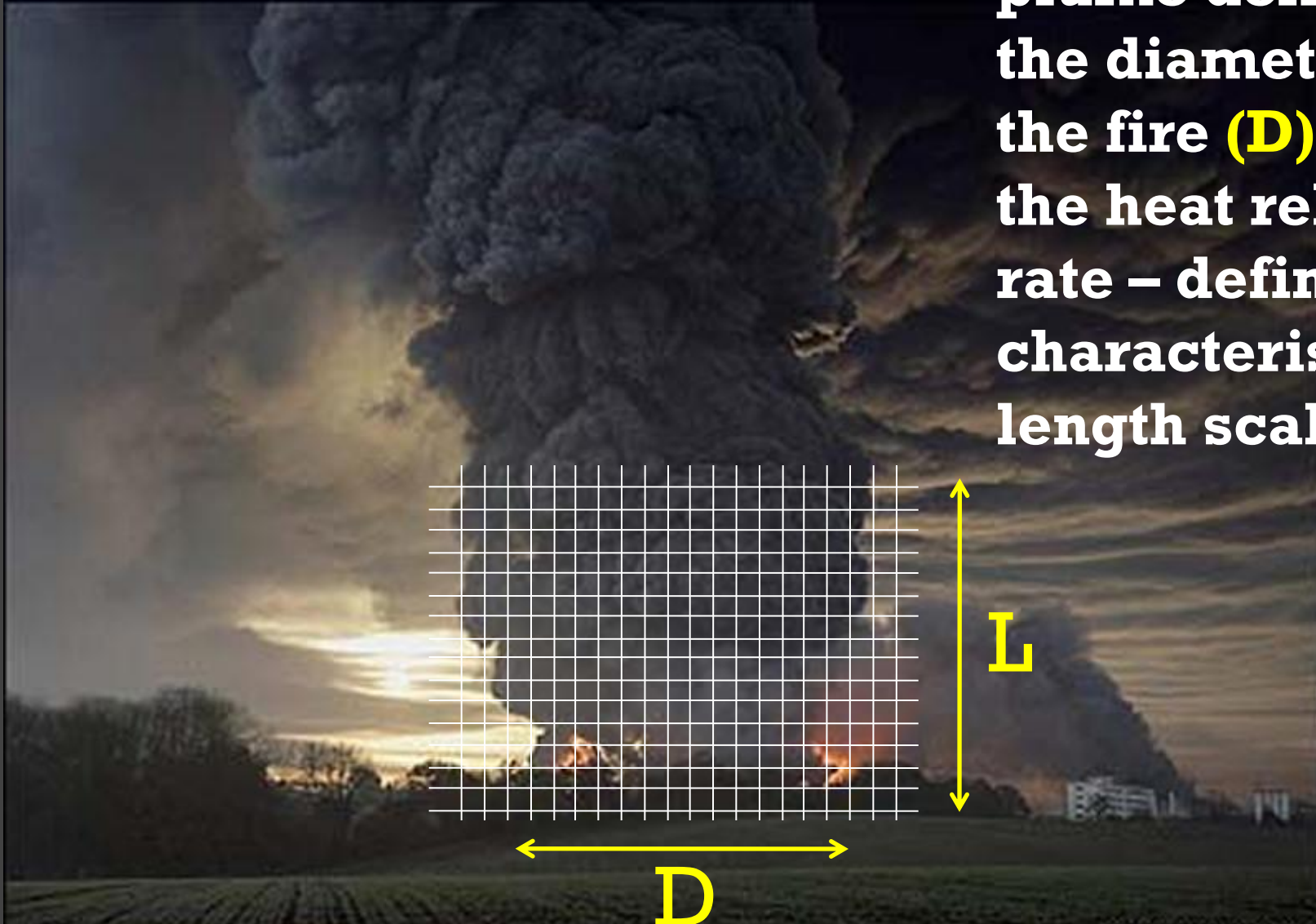
Atmospheric  
and terrain  
variables

- **Dispersion**

- **The fire is treated as a heat source**

# The Plume

- Strength of the plume defined by the diameter of the fire (**D**) and the heat release rate – defines the characteristic length scale (**L**)



# Compatibility

- **Energy/species can be introduced within a defined volume as a source term and allowed to disperse**

# Classic Scaling Approach

- Focuses on proper modelling of buoyant entrainment

$$\underbrace{\rho u \frac{\partial u}{\partial x}}_{\text{Inertia}} \approx \underbrace{\frac{\rho_{\infty} u_b^2}{D}}_{\text{Buoyancy}} \quad \rho g \approx \rho_{\infty} g \quad \rightarrow \quad u_b = \sqrt{gD}$$

$$\underbrace{\rho C_p u \frac{\partial T}{\partial x} \approx \frac{\rho_{\infty} C_p u_b T_{\infty}}{D}}_{\text{Energy Release Rate}} \quad \left. \begin{array}{l} \dot{Q}''' = \frac{\dot{Q}}{D^3} \\ \rho C_p u \frac{\partial T}{\partial x} \approx \frac{\rho_{\infty} C_p u_b T_{\infty}}{D} \end{array} \right\} Q^* = \frac{\dot{Q}_0}{\rho_{\infty} T_{\infty} C_p (gD)^{1/2} D^2}$$

# Use of $Q^*$

$$Q^* = \frac{\dot{Q}_0}{\rho_\infty T_\infty C_{p_\infty} (gD)^{1/2} D^2}$$

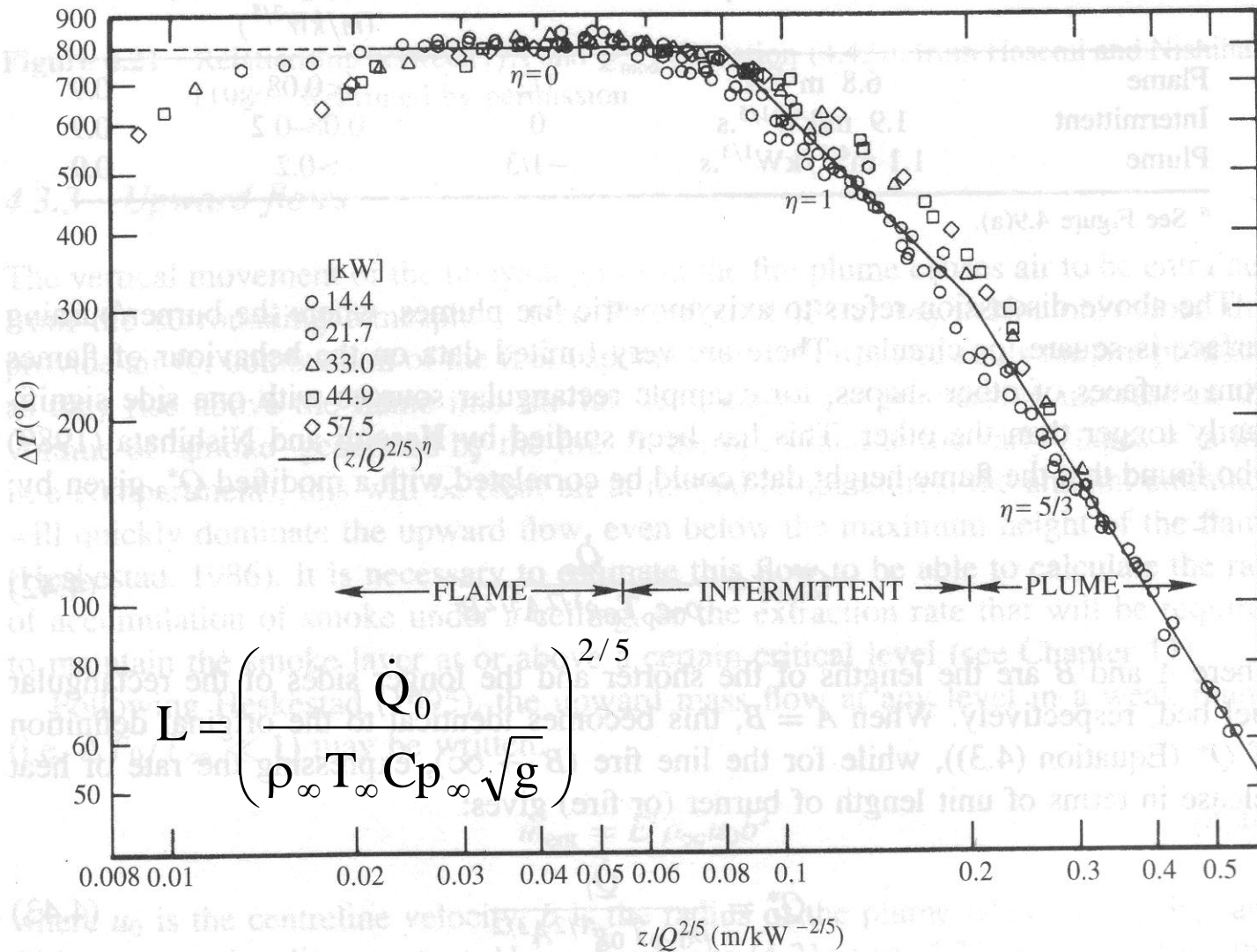
- Obtain a characteristic length scale

- If  $Q^*=1$

$$L = \left( \frac{\dot{Q}_0}{\rho_\infty T_\infty C_{p_\infty} \sqrt{g}} \right)^{2/5}$$

- Temperature and velocity fields can be presented as a function of a scaled length:  
Incorporates the Heat Release Rate Dependency



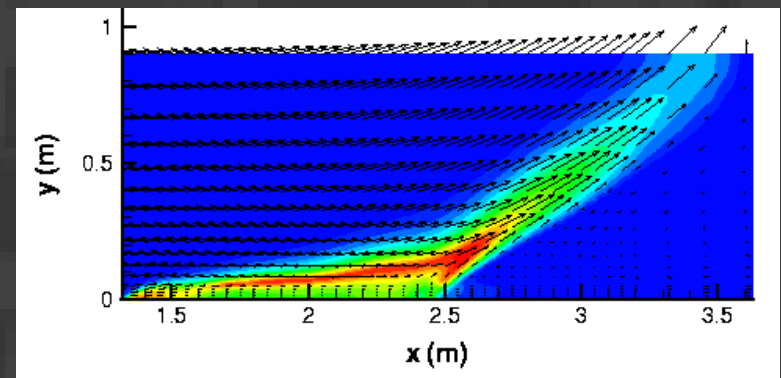
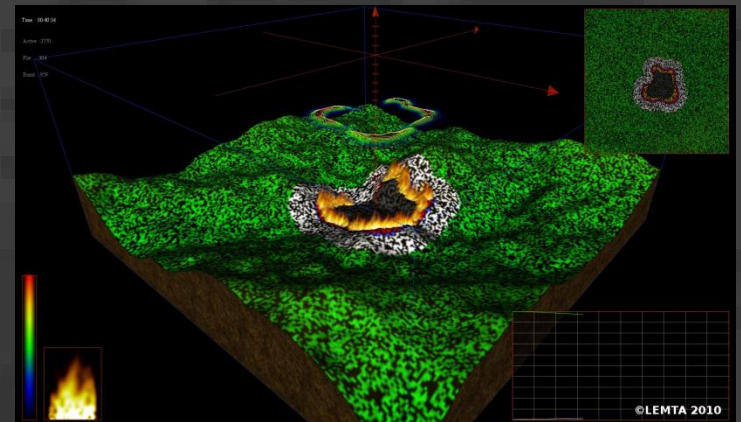
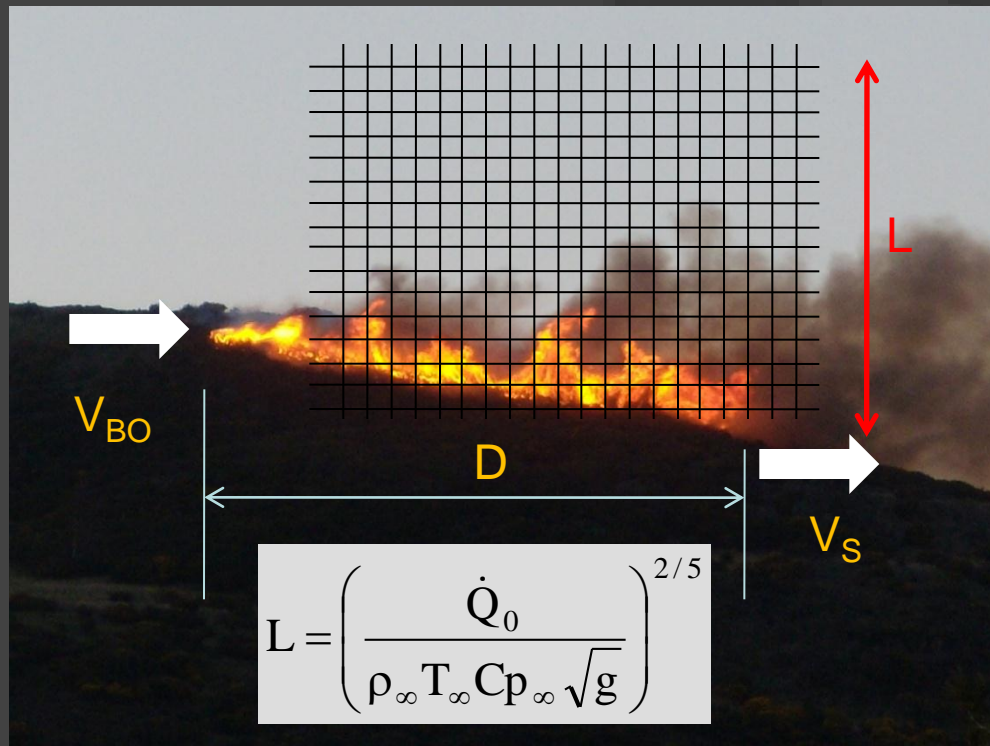


# Compatibility

- In a stationary fire compatibility between the “**entrainment region**” and the “**dispersion region**” can be achieved by a sub grid model that defines the fire as a heat release rate (**source term**) over a well defined “**volume**” (**characteristic length scales (D,L)**)

# Flame Spread

- o Forest fires spread – thus spread rates are necessary
  - o Flame spread rates can be defined in an empirical way and incorporated to “atmospheric type” models – **compatible**
  - o To maintain the characteristic length scale “burn-out” rates are necessary too - **compatible**



# Limitations

- **Flame Spread rates depend on many variables (vegetation type, density, humidity, slope, wind, etc.)**
- **Burn-out rates depend on many variables (vegetation type, humidity, fuel load, density, wind, etc.)**
- **Mixture of fuel and environmental variables**

# Flame Spread: Sequence of Ignitions

10<sup>ths</sup> of  
Metres

To Atmospheric Models

10<sup>ths</sup> of  
Centimetres

Gas Phase Heat  
Transfer

Gas Phase Heat  
Transfer

Combustion  
Processes

Air

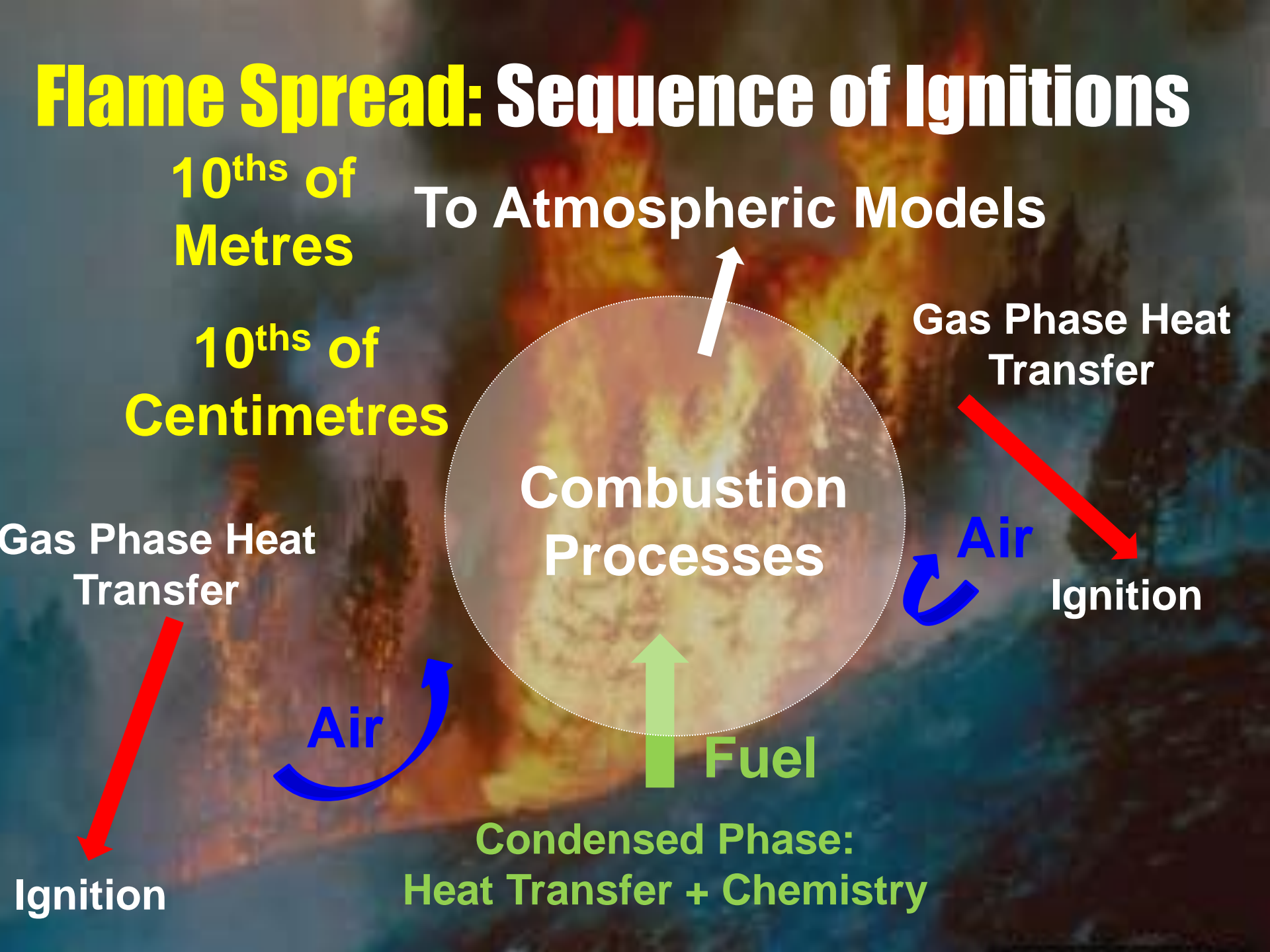
Ignition

Air

Fuel

Condensed Phase:  
Heat Transfer + Chemistry

Ignition





# Incompatible

Fuel Degradation ( $\mu\text{m}$ , s)



Gas Phase Chemistry (nm, ms)



Soot Production ( $\mu\text{m}$ , ms)



Radiative Losses (cm, ns)



Flame Temperature (cm, s)



Radiative Heat Transfer (cm, ns)

# Resolution

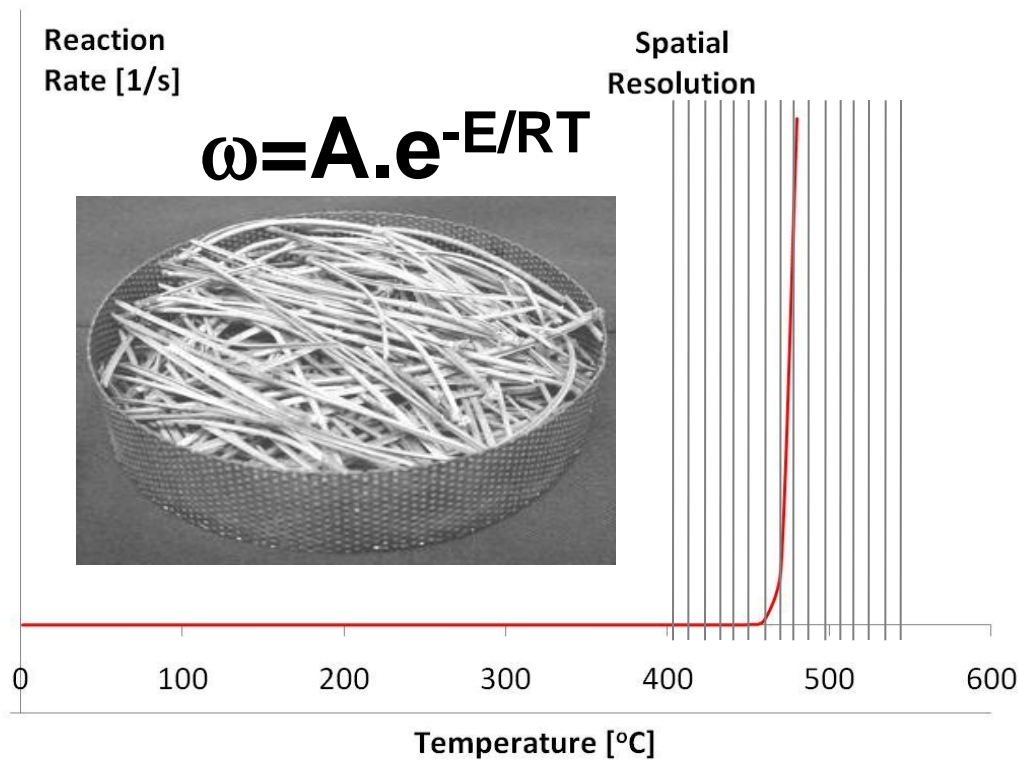
- To resolve ignition it is necessary to resolve the faster time scales and the smallest length scales (**nm, ns**)
- Result needs to be fed into a combustion model ( **$10^{\text{th}}$  cm, sec resolution**) – **Incompatible**
- Computational cost unacceptable – **Precision unnecessary**

# Incompatibility

- Heat fluxes obtained from models/experiments (**10<sup>th</sup>s cm**)
- Heat fluxes applied to a porous matrix (**mm**)
- Temperature across the porous bed resolved (**nm**)
- Degradation resolved via simplified Arrhenius type chemistry ( $\omega = A \cdot e^{-E/RT}$ )
- Experimental validation studies – mass loss (**cm**)



# Why nm Resolution?



- Adequate resolution of the degradation chemistry requires resolving temperature gradients within the fuel thickness

# Compatible Solution

- o **Ideal Scenario:**

- o Input is the gas phase heat flux

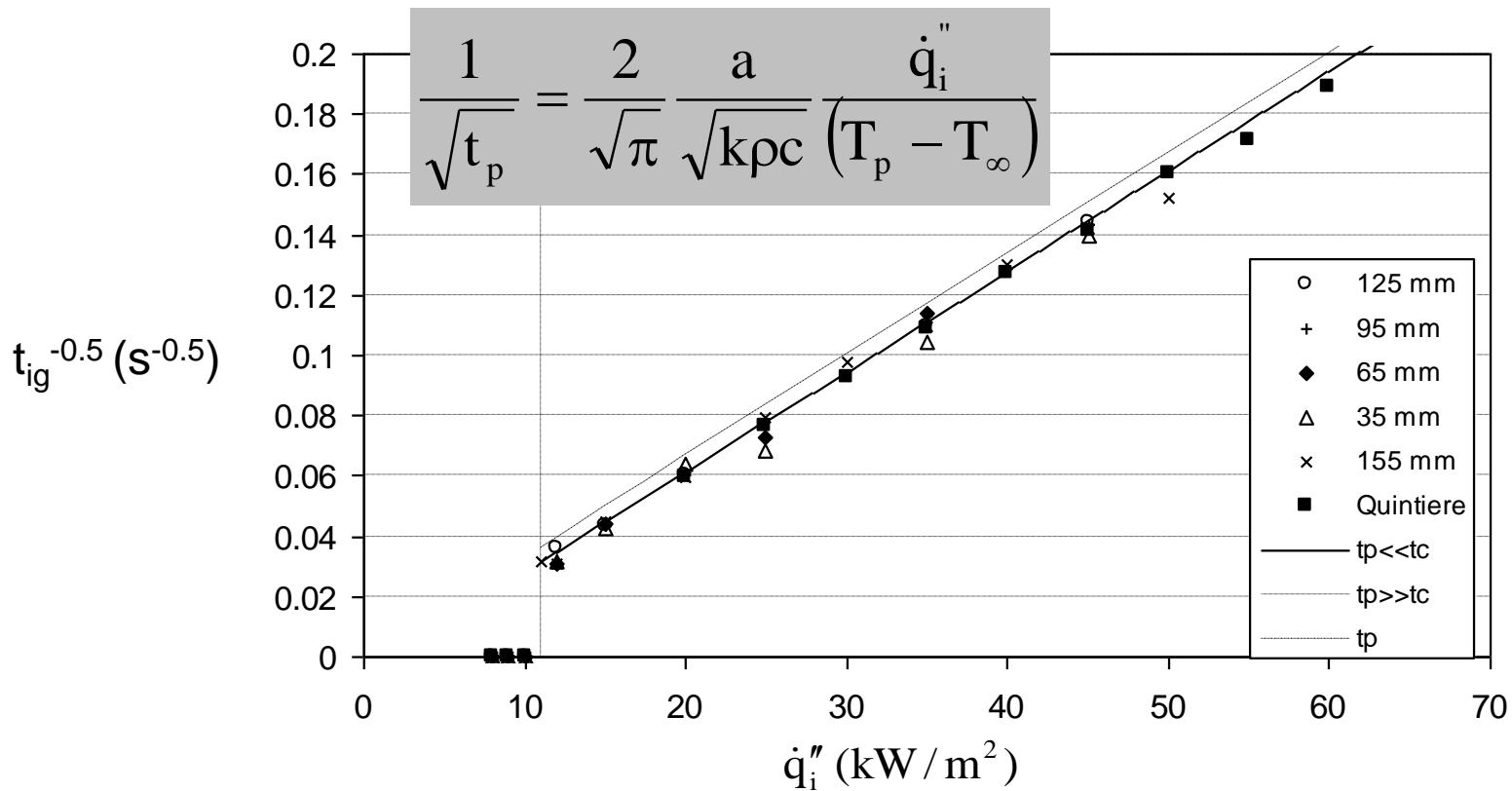
- o Solid phase heat transfer (porous media) does not have to be resolved

- o Degradation chemistry does not have to be resolved

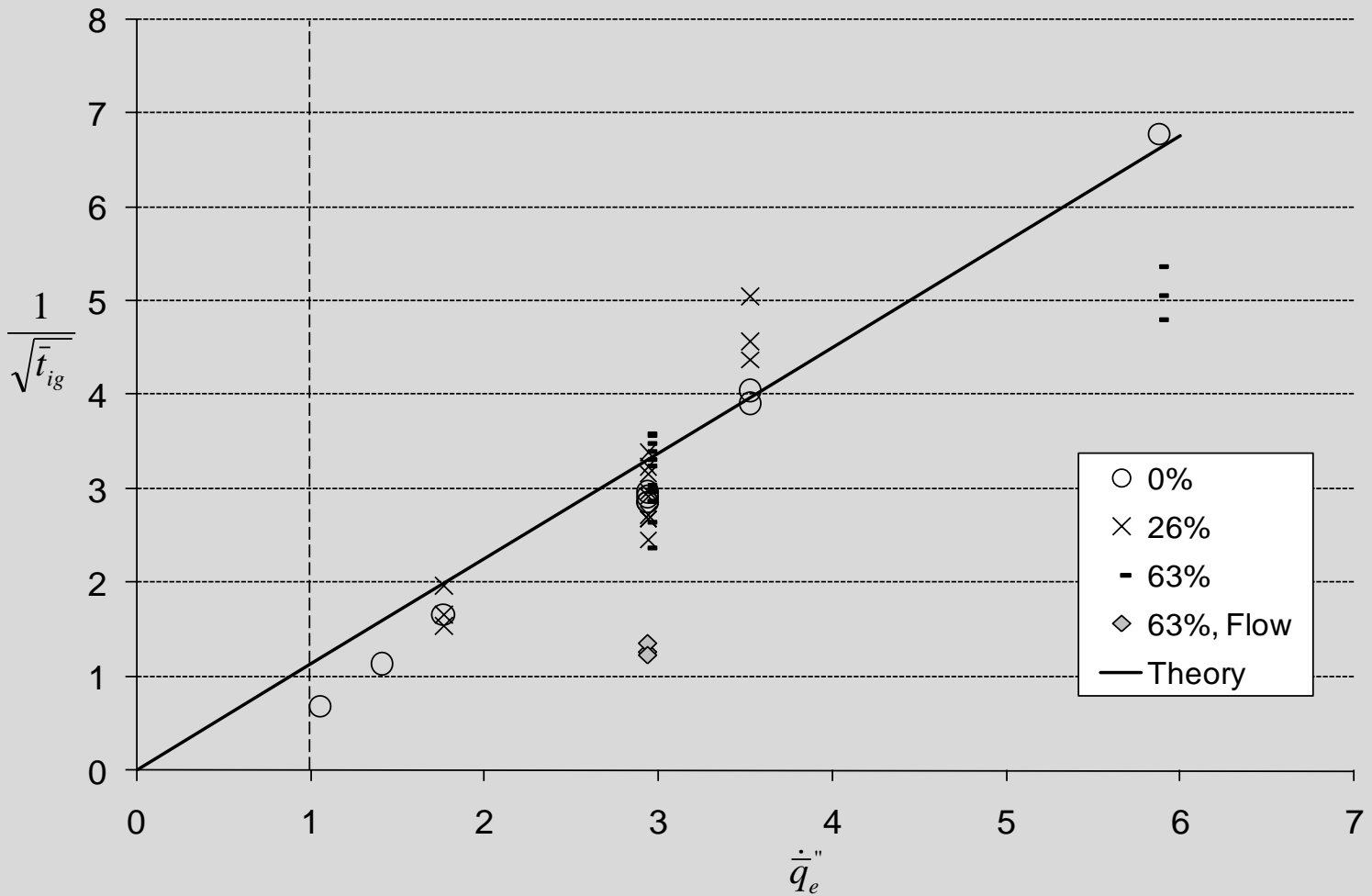
- o **Solution:** Sub-Grid model based on experimental data as an input to the model (**cm/s – resolution**)

# Ignition Delay Time

- Ignition time is linearly dependent to incident heat flux (**cm/s – Model**)



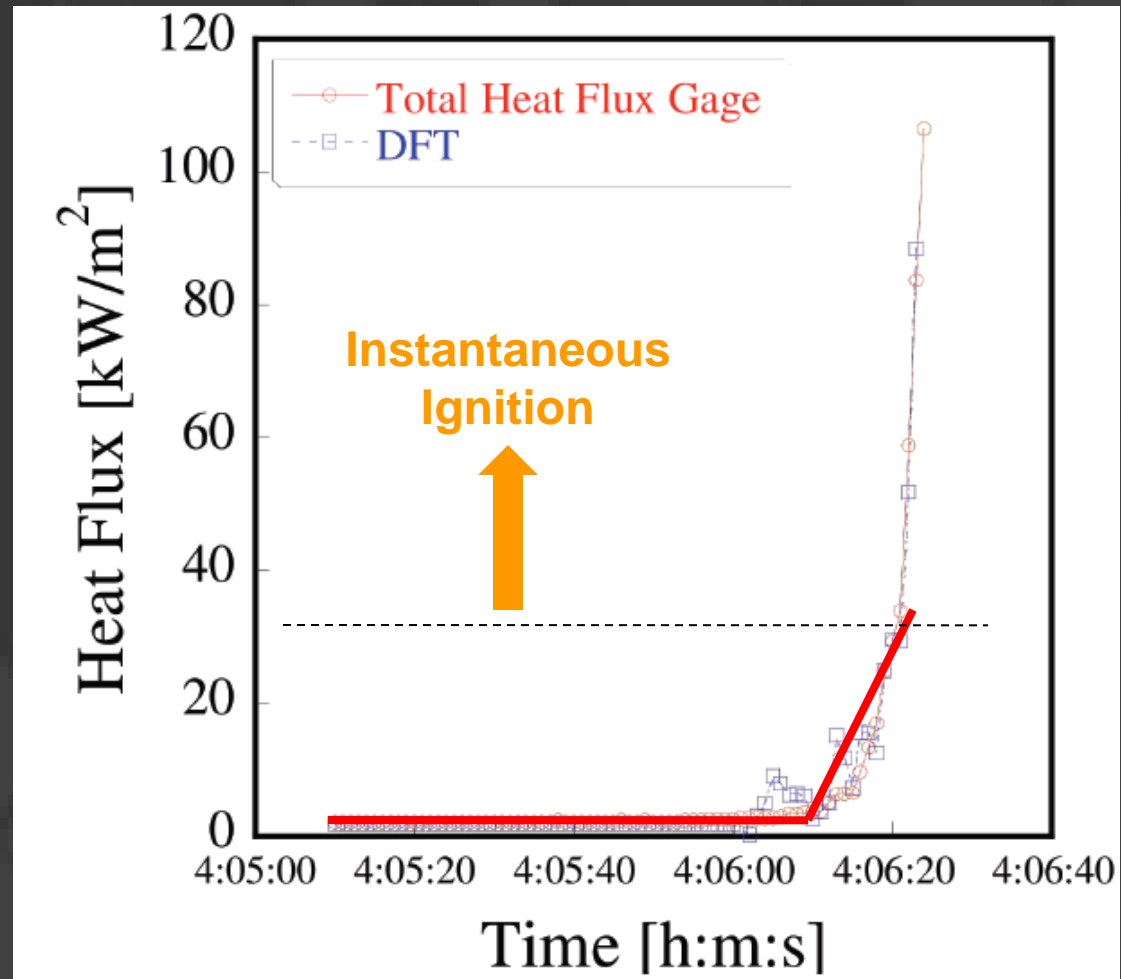
# Applicable to Forest Fire Fuels



# Ignition Delay Times

- Can be estimated as a function of the heat flux if the heat flux is a constant

Manzello, S. L., Park, S. H., Cleary, T. G., Shields, J. R., “Developing Rapid Response Instrumentation Packages to Quantify Structure Ignition Mechanisms in Wildland-Urban Interface (WUI) Fires”, Fire and Materials 2009. 11<sup>th</sup> International Conference Proceedings, San Francisco, CA, 2009, pp. 215–224.

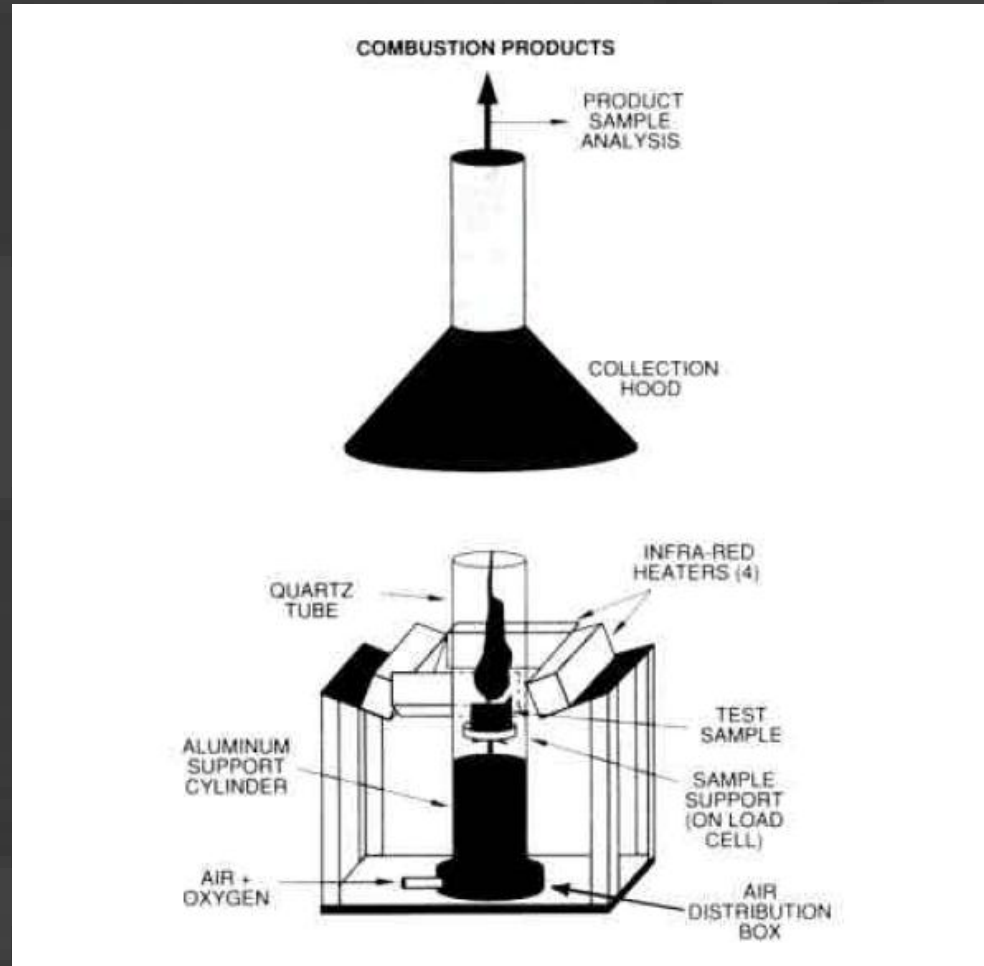
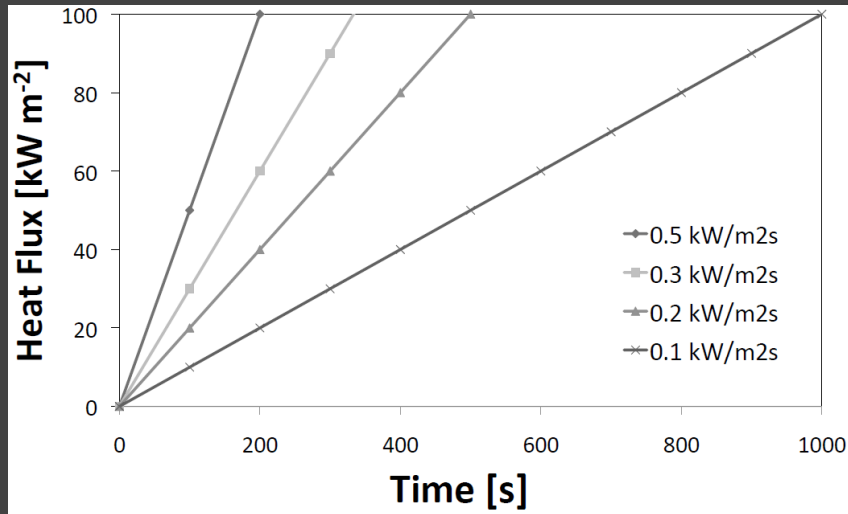


# Modify Mathematical Solution

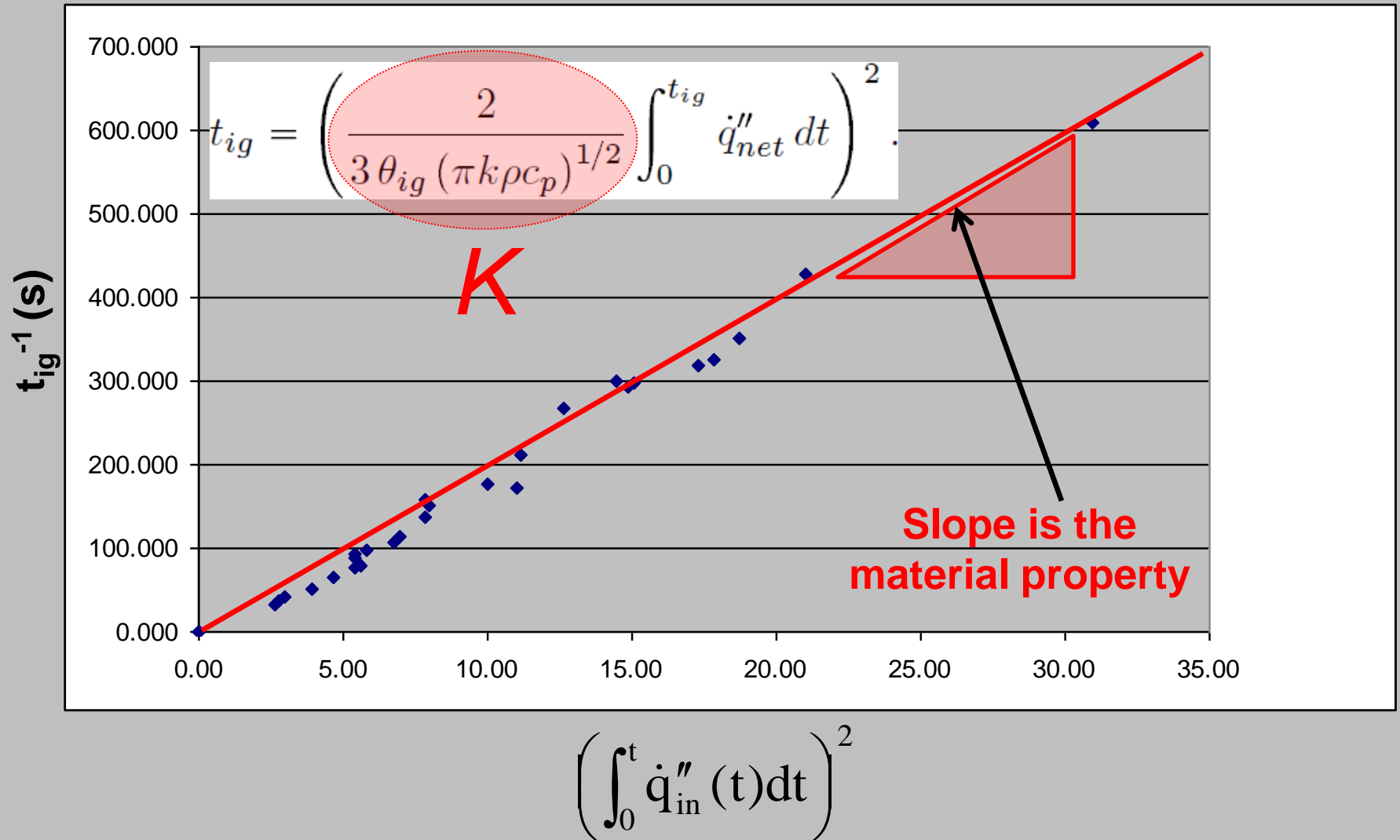
- For linear ramps integrating the expression for time to ignition over time, it can be shown that:

$$t_{ig} = \left( \frac{2}{3 \theta_{ig} (\pi k \rho c_p)^{1/2}} \int_0^{t_{ig}} \ddot{q}_{net} dt \right)^2.$$

# Validation: Fire Propagation Apparatus



# Results





# Compatibility

- **Combustion Model can be used to estimate the evolution of the integral heat flux to the surface as a function of time (10<sup>th</sup>s cm)**
- **“*K*”- material property (fuel type, water content, weather variables, etc.)**
- **Simple model provides  $t_{ig}$**
- **No need to resolve porous media & solid heat transfer or degradation chemistry (nm)**

# Summary

- **Forest fires cover an extensive range of time and length scales**
- **Different processes result in incompatible time and/or length scales**
- **For practical purposes, these need to be resolved with physically based sub-grid models that **ensure compatibility****



**Thank you**